

LABORATORY COMPACTION CHARACTERISTICS OF SOIL



HWA GEOSCIENCES INC.

CLIENT: Glacier North West

SAMPLE ID: PBS-3

PROJECT:

PROJECT NO: 2005097-23

Sampled By: Client

Tested By: EJB

Date Sampled: 1/17/2006

Date Received: 1/17/2006

Date Tested: 1/18/2006

MATERIAL TYPE OR DESCRIPTION:

Permeable Base Stone

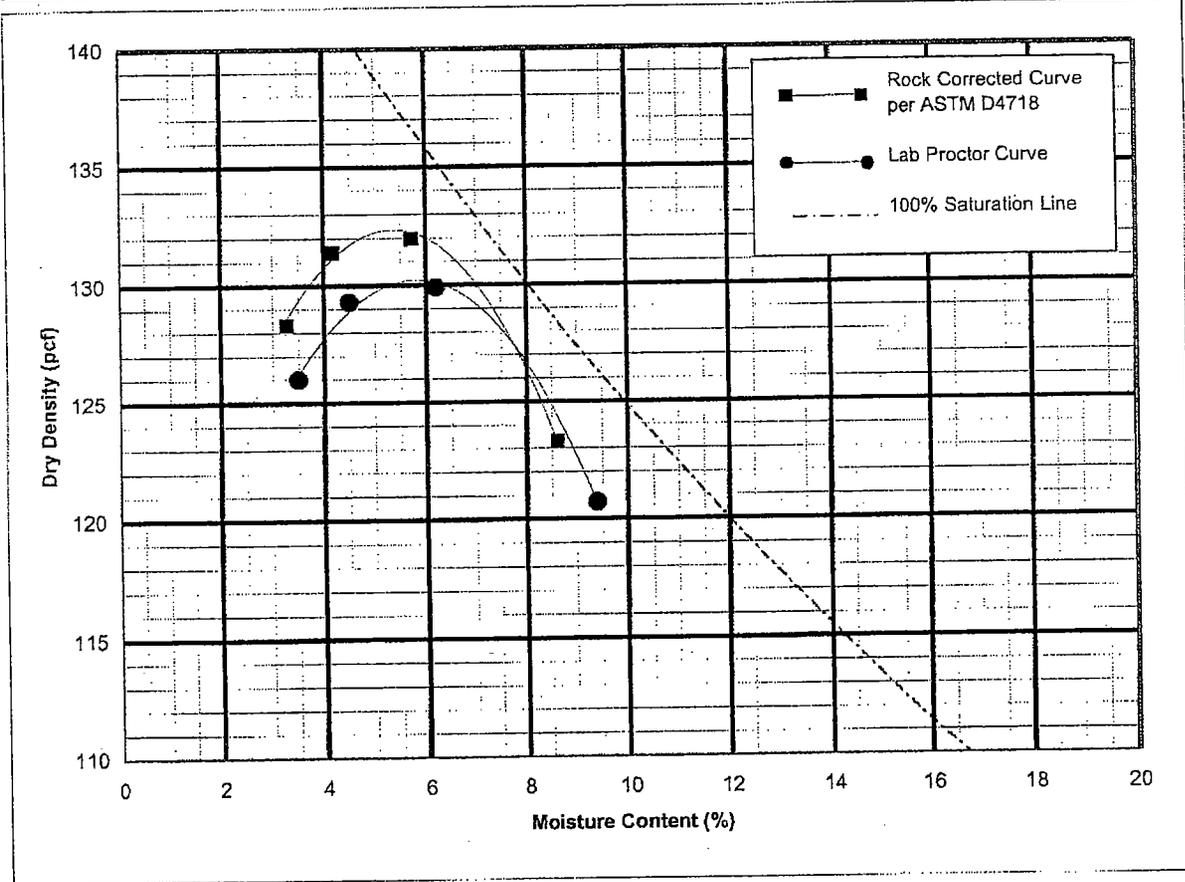
MATERIAL SOURCE, SAMPLE LOCATION AND DEPTH:

Delivered by client

Designation: ASTM D 698 ASTM D 1557 Natural Moisture Content: 3.5 %
 Method: A B C Oversize: 9.3 % retained on: 3/4 in.
 Preparation: Dry Moist Rammer: Auto Manual Assumed S.G.: 2.5

Test Data

Dry Density (pcf)	129.3	129.9	120.7	126.0
Moisture Content (%)	4.5	6.2	9.4	3.5



Data Summary*	
Percent Oversize	9.3%
Max. Dry Density (pcf)*	132.3
Optimum Moisture (%)*	5.3

Test Values At Other Oversize Percentages						
0.0%	5.0%	10.0%	15.0%	20.0%	25.0%	30.0%
130.3	131.4	132.5	133.6	134.8	135.9	137.1
5.7	5.5	5.2	5.0	4.8	4.5	4.3

* values corrected for oversize material per ASTM D4718, using assumed Specific Gravity shown and oversize moisture content of 1%

Reviewed By: JRS **FIGURE 1**

Remold Calculation Form

Project Name: Glacier NW Project #: 2005-097-23
 Sample Designation: Permeable Base Stone Source: DuPont Pit
 Product Number: 8834 Sample #: PBS-3
 Tested By: JRS Date: 01/26/06
 Soil Description: Gray poorly graded coarse gravel with sand (GP)

Maximum Dry Density (pcf):	<input type="text" value="132.3"/>	Optimum Moisture Content (%):	<input type="text" value="5.3"/>
Target Relative Density (%):	<input type="text" value="95"/>	Target Moisture Content (%):	<input type="text" value="5.3"/>
Target Dry Density (pcf):	<input type="text" value="125.7"/>	Target Wet Density (pcf):	<input type="text" value="132.3"/>
Target Sample Height (in):	<input type="text" value="8.00"/>	Target Sample Height (cm):	<input type="text" value="20.32"/>
Target Sample Diameter (in):	<input type="text" value="8.00"/>	Target Sample Diameter (cm):	<input type="text" value="20.32"/>
Target Sample Volume (in ³):	<input type="text" value="402.12"/>	Target Sample Volume (ft ³):	<input type="text" value="0.2327"/>
Target Wet Soil Wt (lbs):	<input type="text" value="30.80"/>	Target Wet Soil Wt (g):	<input type="text" value="13970.2"/>
Lift Thickness (in):	<input type="text" value="2.67"/>	Lift Thickness (cm):	<input type="text" value="6.77"/>
Number of Lifts:	<input type="text" value="3"/>		
Weight per Lift (lbs):	<input type="text" value="10.27"/>	Weight per Lift (g):	<input type="text" value="4656.7"/>

Remolded Sample Data

Sample Height (in):	<input type="text" value="8.00"/>	Sample Height (cm):	<input type="text" value="20.32"/>
Sample Diameter (in):	<input type="text" value="8.00"/>	Sample Diameter (cm):	<input type="text" value="20.32"/>
Sample Volume (in ³):	<input type="text" value="402.12"/>	Sample Volume (ft ³):	<input type="text" value="0.2327"/>
Sample Wt (g):	<input type="text" value="13880.2"/>		
Wet Density (pcf)	<input type="text" value="131.5"/>	Moisture Content (%)	<input type="text" value="5.2"/>
Dry Density (pcf):	<input type="text" value="125.0"/>	Relative Density (%)	<input type="text" value="94.5"/>

HWA GEOSciences Inc. MATERIALS TESTING LABORATORY

Falling Head Permeability Test

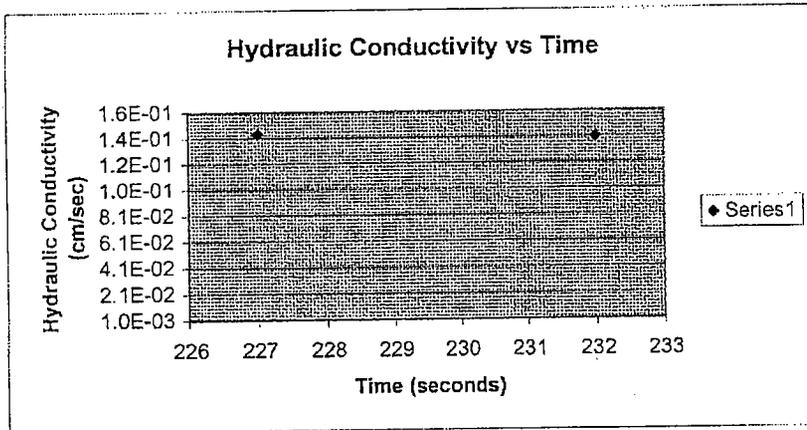
Performed in general accordance with the Army Corps of Engineers EM 1110-2-1906 Laboratory Soils Testing Manual, Appendix VII.

Project:	Glacier NW	Sample No.:	PBS-3
Client:	Same	Sample Source:	DuPont Pit
HWA Project No.:	2005-097-23	Product No.:	8834
Date Sampled:	N/A	Sample Description:	Gray poorly graded gravel with sand (GP)
Sampled By:	Client		
Date Tested:	01/26/06		
Tested By:	JRS		

	Trial Number			
	1	2	3	4
(A) Length of sample (cm):	20.32	20.32		
(B) Initial height of water above datum (cm):	12.7	12.7		
(C) Final height of water above datum (cm):	2.54	2.54		
(D) Total test time (sec):	227	232		
Permeability, k* (cm/sec)	1.4E-01	1.4E-01		
Permeability, k* (in/hr)	204.1	199.7		

* k = { 2.3 (A) Log10 [(B) / (C)] } / (D)

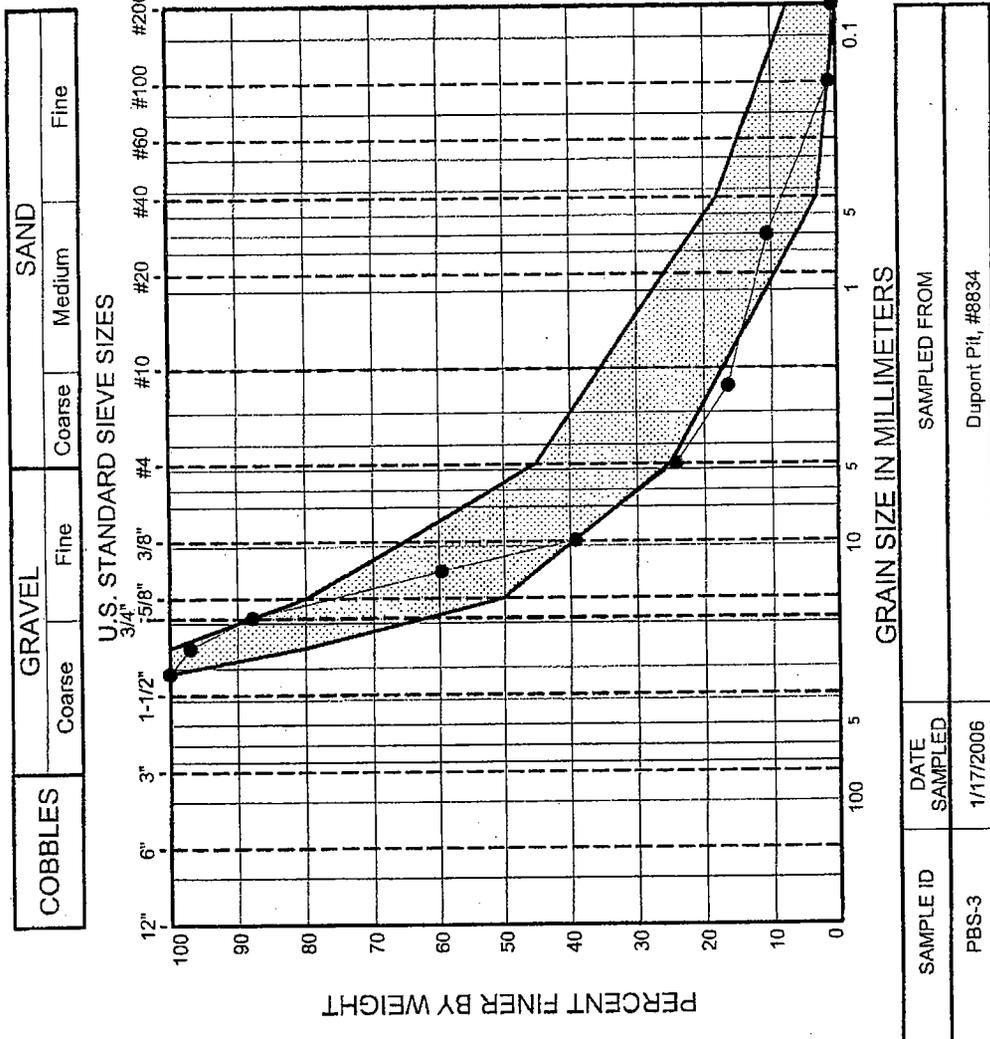
Average Hydraulic Conductivity (cm/sec):	1.4E-01
Average Hydraulic Conductivity (in/hr):	201.9



Porosity Calc's

Project Name: Glacier NW	Project #: 2005-097-23
Tested By: JRS	Date: 02/10/06
Product Designation: Permeable Base Stone	
Product Number: #8834	
Sample #: PBS-3	
<p>Porosity (n) = $1 - \text{Dry Density} / (\text{Specific Gravity} * \text{Unit wt of H}_2\text{O})$</p> <p>n = 0.258</p> <p>Where:</p> <p>Dry Density = 125.0 pcf</p> <p>Specific Gravity is 2.70 (estimated)</p> <p>Unit Wt of Water = 62.4 pcf</p>	

WSDOT 9-03.9(3) CSBC		
Sieve Size	Percent Passing	Specification Limits
8 inch		
7 inch		
6 inch		
5 inch		
4 inch		
3 inch		
2 1/2 inch		
2 inch		
1 1/2 inch		
1 1/4 inch	100.0%	100%
1 inch	97.0%	80-100%
3/4 inch	87.7%	
5/8 inch		50-80%
1/2 inch	59.6%	
3/8 inch	39.1%	
1/4 inch		
No. 4	24.2%	25-45%
No. 8	16.4%	
No. 10		
No. 16		
No. 20		
No. 30	10.6%	3-18%
No. 40		
No. 50		
No. 60		
No. 80		
No. 100	1.2%	
No. 200	0.6%	0.0-7.5%



SAMPLE ID	DATE SAMPLED	SAMPLED FROM
PBS-3	1/17/2006	Dupont Pit, #8834
MATERIAL CLASSIFICATION / DESCRIPTION		
Permeable Base Stone		
Moisture %	L.A. Abrasion %	Degradation Ratio
2.5		
		MgSO ₄ Plastic Fracture Index %

SIEVE ANALYSIS OF AGGREGATE METHOD ASTM C136

Glacier Northwest





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Date Received January 17, 2006

Date Reported February 10, 2006

Sample Number PBS-3

Source Glacier Northwest, DuPont Pit

Product Description Permeable Base Stone

Product Number #8834

Gravel Distribution Analysis (ASTM C 136)

Sieve Size		Sample	Specification
		Percent Passing	
1 1/4"	31.5 mm	100	100
1 inch	25.0 mm	97	90-100
3/4 inch	19.0 mm	87.7	80-100
1/2 inch	12.5 mm	59.6	50-80
3/8 inch	9.5 mm	39.1	40-60
No. 4	4.75 mm	24.2	20-40
No. 8	2.36 mm	16.4	15-30
No. 30	0.60 mm	10.6	5-20
No. 100 (wet)	0.15 mm	1.2	2-10
No. 200 (wet)	0.075 mm	0.6	2-6

Infiltration Rate Inches/Hour	Compaction % Proctor	Total Porosity	Percent Fracture
Corp Of Engineers EM 1110-2-1906 Appendix VII	ASTM D 698 Standard Proctor	Calculated	WAQTC TM 1 (Supercedes WSDOT 106)
202	94.5	0.258	96

Reviewed by: John M. Sals

Sand Point Magnuson Park
 Synthetic Turf Fields
 Lateral Drainage Rate Estimate

Alternate Design with Four Equally Spaced Drainage Laterals - 8" Aggregate Depth

All drainage from the synthetic turf field areas will be collected by 4 lateral drain lines in the
 vertical percolation through the synthetic turf and the permeable aggregate layers
 lateral percolation through the permeable aggregate across the field width to the perimeter drain
 vertical percolation through the pea gravel backfill
 pipe flow through the drainage collector to the onsite storm system or daylight locations

Reach Type	Surface Description	Permeability "k" (ft/min)	Length Feet	Gradient	Velocity (ft/min)	T of C (min)
AB	Percolation Turf	.0970	0.15	1.00	0.097	1.55
BC	Percolation Aggregate	.7087	0.00	1.00	0.709	.00
	Gradient Buildup - assume earlier storm - no time					
CD	Percolation Aggregate	.7087	79.00	0.013	0.009	8575.21
DE	Percolation Pea Gravel	9.3388	1.50	1.00	9.339	0.16

Total Tc = **8576.92** Minutes
 142.95 Hours
 5.96 Days

Synthetic Turf System Permeability

Testing performed on other synthetic turf surfaces indicated a drainage rate of approximately 70 inches/hour
 This corresponds to a rate of 0.097 feet per minute

Aggregate Permeability

The permeability of the aggregate is estimated with the 10th percentile particle size. Based on sieve testing from the primary supplier, the 10th percentile particle size typically ranges around the #30 sieve.

The permeability rate is calculated as follows:

$K=100(DxD)$ where D = 10th % particle size in cm and K= permeability in cm/sec

- D = 0.06 cm
- K = 0.36 cm/sec
- K = 0.7087 ft/min

Gradient Build Up

For the purposes of this calculation, a 1/2% gradient associated with the subgrade slope and the aggregate is assumed to be saturated to the full depth of 8 inches resulting in a hydraulic grade of 1.3%.

Lateral Percolation

This is calculated with Darcy's Law where the flow velocity is the product of the permeability rate and the gradient.

Sand Point Magnuson Park
 Synthetic Turf Fields
 Lateral Drainage Rate Estimate

Current Design with Subsurface Drainage System (15' o.c. Drainage Laterals) 10.25" Aggregate Depth

There will be no surface runoff from the sythetic field areas. All drainage from the synthetic turf field areas will be collected by the subsurface drainage system. The drainage path for these areas is comprised of the following:

- vertical percolation through the synthetic turf and the permeable aggregate layers
- lateral percolation on a gradient through the permeable aggregate to the subsurface drainage trench
- vertical percolation through the pea gravel backfill
- pipe flow through the subsurface drainage system to the onsite storm system or daylight locations

Reach Type	Surface Description	Permeability "k" (ft/min)	Length Feet	Gradient	Velocity (ft/min)	T of C (min)
AB	Percolation Turf	.0970	0.15	1.00	0.097	1.55
BC	Percolation Aggregate	.7087	0.85	1.00	0.709	1.21
Gradient Buildup - assume earlier storm - no time						
CD	Percolation Aggregate	.7087	9.00	0.04	0.028	317.50
DE	Percolation Pea Gravel	9.3388	1.50	1.00	9.339	0.16

Total Tc = 320.41 Minutes
 5.34 Hours

Synthetic Turf System Permeability

Testing performed on other synthetic turf surfaces indicated a drainage rate of approximately 70 inches/hour This corresponds to a rate of 0.097 feet per minute

Aggregate Permeability

The permeability of the aggregate is estimated with the 10th percentile particle size. Based on sieve testing from the primary supplier, the 10th percentile partical size typically ranges around the #30 sieve.

The permeability rate is calculated as follows:

$K=100(DxD)$ where D = 10th % partical size in cm and K= permeability in cm/sec

- D = 0.06 cm
- K = 0.36 cm/sec
- K = 0.7087 ft/min

Gradient Build Up

For the purposes of this calculation, a 4 inch gradient is assumed to be already inplace between each of the subsurface drainage trenches. This would be the case with successive storm events. If a gradient is not in place, the time of concentration would be significantly longer due a flatter gradient.

Lateral Percolation

This is calculated with Darcy's Law where the flow velocity is the product of the permeability rate and the gradient.